# A two-dimensional laser-wire scanner for electron accelerators 

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#### Abstract

A two-dimensional laser-wire scanner capable of measuring the transverse charge profiles of an electron (or positron) bunch has been constructed at the PETRA accelerator in DESY. The development of the system is explained in this paper, along with descriptions of its photon detector and laser system. Results of transverse profile scans are presented for both horizontal and vertical directions. The measurement error is $1.3 \%$ from a multi-scan measurement in the vertical direction, where single scans can be performed in less than 50 s .


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## 1. Introduction

Laser-based beam profile monitors, and in particular the laser-wire (LW), will be needed to measure electron (or positron) beam sizes for future synchrotron light sources [1] and electron-positron colliders [2]. Due to the small emittance and high power requirements of these machines, the use of traditional profiling methods such as wire scanners or screens is limited [3]. For these reasons, LWs will be essential to monitor the transverse emittance at future electron accelerators. The results presented in this paper were obtained using a positron beam, all the conclusions are also applicable to electron beams.

The LW is based on inverse Compton scattering (e $\gamma \rightarrow \mathrm{e} \gamma$ ) between the electrons and laser photons [3]. By counting the number of Compton scattered photons produced as a function of the laser position, it is possible to reconstruct the spatial distribution of the electron bunch. Due to the low rate of the inverse Compton scattering

[^0]process, the LW is inherently a non-invasive profiling technique [4]. Furthermore, it has a much improved resolution [5], faster profiling speed [6] and does not suffer from the mechanical issues of traditional wire scanners.

This paper describes the upgrade of the one-dimensional (vertical profiling) LW tested previously at PETRA [7] to a two-dimensional (2D) bunch profiler, where the laser beam can be sent to collision in either the horizontal or the vertical direction alternately, enabling it to perform a vertical profile (VP) or horizontal profile (HP) measurement, respectively. New capabilities of the LW, such as electron beam finding, fast scanning and longitudinal scanning are also discussed. This work is complementary to the R\&D currently ongoing at the accelerator test facility (ATF) at KEK [5], where the emphasis is on scanning with very small laser spot-sizes.

## 2. Experimental setup

Fig. 1 shows a plan overview of the LW experimental layout on the east bending arc of the PETRA ring. It illustrates the major components of the LW system; high power laser, optical scanning systems, beam position monitor (BPM) and Compton calorimeter. The laser pulse


Fig. 1. Overview of the LW setup. A detailed schematic of the vertical breadboard is shown in Fig. 2.
collides with the positron bunch within a custom built vacuum vessel with optical view ports for laser light. The point where the laser light intersects the positron bunch is defined as the interaction point (IP) which is not fixed but depends on the positron beam orbit. The Compton photons and charged beam are separated by a downstream dipole magnet. After separation the Compton photons exit the PETRA beam pipe through a 6 mm thick Aluminium window before reaching the calorimeter. The positron beam position is measured using a standard PETRA four button pick-up BPM.

A commercially available neodymium-doped yttrium aluminium garnet (Nd:YAG) laser system was used to produce the high power light pulses required for Compton scattering. The high power laser beam was transported from the laser hut to the interaction area inside the PETRA tunnel through an existing access pipe. The total transport distance was about 15 m and the transport optics used a one-to-one imaging Gaussian telescope consisting of two 5 m focal length lenses separated by a 10 m distance. Having passed through the Gaussian telescope arrangement, the laser beam reached the 2-D vertical LW breadboard mounted around the PETRA beam pipe, where it was then guided onto a 3 -times magnification beam expander. Fig. 2 shows a schematic illustrating the technical features of the LW optical scanning system, and Fig. 3 shows a photograph of the LW optical scanning system in place on PETRA. The beam expander is configured to increase the laser beam diameter to 25 mm and collimate it. The laser beam is then guided to one of two scanning systems (one for each transverse profile) via the use of a motorized flipping mirror. The scanning systems are identical in design, and are arranged so that one is rotated $90^{\circ}$ relative to the other about the IP; a schematic of the vertical scanning system is shown in Fig. 4.

### 2.1. Scanning system

The scanning systems contain a piezo-driven mirror, to deflect the laser beam, and a commercially available


Fig. 2. Schematic of the LW optical scanning system. The $x$ - and $y$-axes are normal to the positron beam trajectory. A close up of the VP scanning system is shown in Fig. 4.
convergent lens (CVI LAP 250) with a focal length of 250 mm , which focuses the beam down to a laser spot size $\sigma_{0}=4.5 \mu \mathrm{~m}$, where $\sigma_{0} \equiv W_{0} / 2$. The scanning systems are mounted on translation stages to allow movement of the focused laser spot in the transverse plane of the positron bunch, as indicated in Fig. 4. The lens is also mounted on a
small translation stage that moves parallel to the axis of laser propagation; this allows the focus position of the laser beam to be changed.

The scanning mirror is a 2 in . multilayer coated mirror ( $99.9 \%$ reflective at 532 nm ). It is mounted on a piezoelectric stack which can be deflected by a maximum angle of approximately 2.5 mrad (with an applied voltage of 100 V ). By rotating the piezo-driven mirror by an angle $\theta$ the laser beam is steered by an angle $2 \theta$. The shift in transverse position of the focus ( $\Delta$ ) obtained when a laser beam is deflected by angle $2 \theta$ at the input of a focusing lens (with focal length $f$ ), is given by: $\Delta=2 f \theta$. Given the 250 mm focusing lens and the maximum deflection of 2.5 mrad by the piezo-driven mirror, the total maximum


Fig. 3. Photograph of the LW optical scanning system.
scanning range was 1.25 mm . In addition, the beam finding translation stage can be used for shifting the position of the laser focus; providing a complementary method for scanning larger ranges than permitted by the piezo-electric system.

### 2.2. Post IP

As the laser beam travels past the IP it becomes divergent and needs to be refocused by a convergent lens (CVI LAP 125) for imaging. The lens has a focal length of $f=125 \mathrm{~mm}$ and images the plane of the IP on to a CCD camera. The magnification factor of this arrangement is 8.3 and is determined by the ratio of the optical distance between the lens and the CCD camera to the optical distance of the IP to the lens [8,9]. Two such identical post IP imaging systems were constructed, one for each profiling axis. An overview of the optical path from the output of the beam expander to the post IP CCD camera is shown in Fig. 5. An image of the laser intensity profile was taken at the post IP location, using a laser diagnostic camera (Gentec WinCamD) and is shown in Fig. 6. The analysis indicates that the post IP beam radius $W_{M} \simeq 75 \mu \mathrm{~m}$, which is magnified by the factor of 8.3 discussed above. Therefore the true spot size at the IP is $W_{0} \simeq 9 \mu \mathrm{~m}$. This is in good agreement with the ABCD matrix calculation shown in Fig. 5.

### 2.3. Laser system

The LW laser system must be capable of producing high power light pulses with good transverse and longitudinal mode quality. The laser system is injection seeded to eliminate longitudinal mode-beating; an effect which


Fig. 4. Schematic of the vertical profile scanning system, which contains the piezo-driven mirror and focusing lens.


Fig. 5. Plot of the ABCD matrix calculated beam size from the beam expander to the post IP CCD camera, taking into account the mode quality factor of the laser $\left(M^{2}\right) . W_{0}$ is the laser spot radius as described in Section 2.3.1.


Fig. 6. Laser pulse image taken using CCD profiling equipment in the post IP section of the LW system.
creates temporal sub-structure within the laser pulse at the level of 100 ps . This is the same order of magnitude as the positron bunch length and therefore makes beam-size measurement more statistically challenging; the
elimination of mode-beating is thus important for making fast scans [7]. To illustrate the effect of the seeding process on the longitudinal profile of the laser pulse, scope traces of the output of a photodiode are shown for


Fig. 7. Oscilloscope trace of the laser pulse as measured by a fast photodiode (rise time $\sim 1 \mathrm{~ns}$ ) when the laser was unseeded (a) and seeded (b).

Table 1
Summary of laser properties

|  | Value | Units |
| :--- | :--- | :--- |
| Pulse energy at 532 nm | $60 \pm 5$ | mJ |
| Peak power at 532 nm | $12 \pm 1$ | MW |
| Repetition rate | 20 | Hz |
| Pulse duration | $5 \pm 1$ | ns |
| RMS pulse jitter (rel. to ext. trigger) | 1 | ns |
| Mode quality factor $\left(M^{2}\right)$ | $2.68 \pm 0.05$ |  |
| Horizontal angular jitter | 18.8 | $\mu \mathrm{rad}$ |
| Vertical angular jitter | 9.4 | $\mu \mathrm{rad}$ |

the laser system unseeded and seeded in Figs. 7(a) and (b), respectively. A commercially available injection seeded Qswitched Nd:YAG laser capable of delivering 12 MW light pulses at 20 Hz was chosen. Such a high power was needed in order to generate a sufficient number of Compton events per laser pulse as described in Section 3.

The fundamental wavelength produced by the Nd:YAG laser is 1064 nm , which is frequency doubled (using a second harmonic generating crystal) to obtain a wavelength of 532 nm . This process is not $100 \%$ efficient and the remnant 1064 nm light component is separated using dichroic mirrors and dumped. Adjustment of the intensity of the laser light was achieved by rotating the polarization of the laser light relative to a Brewster plate using a halfwave plate. A summary of the laser characteristics is presented in Table 1.

### 2.3.1. Transverse mode: $M^{2}$ measurements

The laser beam propagates with radius described by the formula
$W(z)=W_{0}\left[1+\left(\frac{M^{2} \lambda}{\pi W_{0}^{2}} \cdot z\right)^{2}\right]^{1 / 2}$
where $W(z)$ is the laser spot radius (distance from the center of the distribution to the position where the intensity drops by a factor $\mathrm{e}^{-2}$ ), $W_{0}$ is the minimum laser waist, $\lambda$ is the laser wavelength and $M^{2}$ is a factor $\geqslant 1$ which describes the quality of the real beam compared to an ideal $\mathrm{TEM}_{00}$ Gaussian beam (for which $M^{2}=1$ ) [8].

The $M^{2}$ of the laser beam was measured by focusing it with a plano-convex lens of focal length 500 mm . CCD images of the laser beam were recorded using the WinCamD at a range of distances from the focusing lens. The beam radius data as a function of camera position are plotted in Fig. 8 and fit using Eq. (1). The $M^{2}$ obtained from the fit was $2.68 \pm 0.05$. This value is compatible with the measured waists of $W_{\text {input }}=12.5 \mathrm{~mm}$ and $W_{0}=9 \mu \mathrm{~m}$ using the following formula:
$W_{\text {input }} W_{0}=M^{2} \cdot \frac{\lambda f}{\pi}=\mathrm{constant}$
where $\lambda$ is the wavelength of the laser light [8]. Given that $W_{\text {input }}=12.5 \mathrm{~mm}, f=250 \mathrm{~mm}$ and $\lambda=532 \mathrm{~nm}$, Eq. (2) gives $W_{0} \simeq 9 \mu \mathrm{~m}$, which is consistent with the post-IP CCD camera measurements described in Section 2.2. As $W_{0}=2 \sigma$, this gives $\sigma=4.5 \mu \mathrm{~m}$.

### 2.3.2. Pointing jitter measurement

The laser system produces light pulses with a natural angular jitter, or pointing instability. Knowledge of this jitter is required in order to determine the contribution of such an effect to beam size measurements. In order to determine its pointing stability, the laser was focused using a 1 m focal length lens onto an industrial digital camera


Fig. 8. Measurement of $M^{2}$ using a $f=500 \mathrm{~mm}$ lens. The fit equation is given in Eq. (1). The fit gives $M^{2}=2.68 \pm 0.05$.
(with pixel size $6.7 \mu \mathrm{~m}$ ) and successive laser shots were measured. To create a pedestal, 100 images were taken of the ambient light (no laser) and averaged. This was subtracted from each of a further 100 images taken with the laser firing. Each background subtracted image is projected on to the $x$ and $y$-axes and fit to a Gaussian, the fit centroids are plotted in Fig. 9.

From Fig. 9, the pointing jitter is measured to be $18.8 \mu \mathrm{rad}$ in the horizontal direction and $9.7 \mu \mathrm{rad}$ in the vertical direction; this difference is a property of the laser. The vertical angular jitter gets transformed by the light transport optics into a position variation along the positron beam direction and therefore is irrelevant. The horizontal angular jitter is correspondingly transformed into a position variation at the IP parallel to the scanning direction. The combination of the 3-times magnification telescope and 250 mm focusing lens thus results in a position jitter ( $\sigma_{\text {jitter }}$ ) at the IP of $1.6 \mu \mathrm{~m}$ for both VP and HP measurements.

### 2.3.3. Laser synchronization

PETRA provides two TTL-level signals for synchronizing the laser to the positron bunches, a $96 \mathrm{~ns}(10.42 \mathrm{MHz})$ bunch clock and a $7.68 \mu \mathrm{~s}(130.2 \mathrm{kHz})$ revolution clock. The timing jitter of the bunch clock and the revolution
clock with respect to the BPM signal at the LW IP is negligible compared to the timing jitter of the laser relative to the revolution clock.

A custom designed VME-based trigger card ("LT2") supplies the laser with a Fire signal, to fire the flash-lamps, and a Q-switch signal that operates the Pockels cell and allows light out of the laser. A timing overview is shown in Fig. 10. The LT2 trigger card can adjust the revolution clock to Q -switch timing in steps of 0.5 ns to synchronize the laser pulse, of width 5 ns , with the positron bunch. The stability of the LT2 output is dependent upon the stability of the timing signals from PETRA. The Fire to Q-switch time is adjusted using a fast rise-time photodiode to look at the light output of the laser, and the time adjusted until a peak in the output is found, typically of order $182.5 \mu \mathrm{~s}$. Both the Fire and Q-switch signals are then adjusted together relative to the revolution clock to synchronize with the positron bunch at the IP.

### 2.4. Photon detector

The photon detector is made of nine lead tungstate crystals organized in a $3 \times 3$ matrix. This is optically connected to a photo-multiplier (PMT) which amplifies the output from the lead tungstate crystals. The detector is


Fig. 9. Histograms showing the distribution of laser spot in the horizontal (a) and vertical (b) axes of the digital camera.


Fig. 10. Schematic summarizing the synchronization signals for the LW DAQ.
housed within an arrangement of lead blocks which serves to protect against synchrotron and other low energy radiation.
The calorimeter was tested in the DESY Test Beam 24 beam line, and exposed to single electrons of various energies. The calorimeter voltage output was recorded on digital sampling oscilloscope for 500 ns triggered just before beam arrival. A minimum of 10 scope measurements


Fig. 11. The mean peak signal from the PMT is plotted against the electron test-beam energy.
were taken for each particle energy and PMT voltage setting. The mean peak signal from the PMT was determined for different beam energies at a fixed PMT voltage of -1115 V . This is plotted in Fig. 11 and shows that the calorimeter response is linear. Further details of this work can be found in Refs. [9,10].

### 2.5. The data acquisition system

An overview of the data acquisition system (DAQ) is shown in Fig. 12. It uses a National Instruments (NI) M-series high-speed multifunction DAQ card for the analogue-to-digital and digital-to-analogue conversion (ADC and DAC). The DAQ software is written using NI LabVIEW, for both the control of the LW and the online analysis of the data. Customized modules are used for control of the piezo scanner and calorimeter output conditioning.

The DAQ is triggered by a signal from LT2 that has the same timing as Laser Fire. A counter (CTR0) is triggered by this signal and counts for a specific time delay, CTR0 delay, after which the CTR0 output goes high for the duration of the CTR0 pulse, which opens the window for the peak detector, and starts a second counter (CTR1). CTR1 counts for the CTR1 delay and then rises, causing the two ADC channels (for the peak detector and the piezo amplifier monitor) to be read on this edge. When CTR0 falls, this triggers the DAC to output its next value.


Fig. 12. Schematic of the LW data acquisition system.

The DAQ then resets both counters and waits for the next Fire signal.

The DAQ system also controls the translation stages used for beam-finding and focus position movement described in Section 2.1.

## 3. Data taking and results

The following data were taken using PETRA set with the standard HERA injection optics with one positron bunch, at a current of 0.5 mA and a beam energy of 6 GeV . For these beam settings and the laser parameters described in Section 2.3, the number of Comptons generated per laser pulse is approximately 1100 for the VP and 120 for the HP [3,9]. The data was taken in dedicated fills, but the LW could also be run parasitically during synchrotron radiation runs for HASYLAB.

The LW can operate two types of scan enabling it to perform bunch size measurements spanning over three orders of magnitude (from $10^{-5}-10^{-2} \mathrm{~m}$ ):

- Ramp scan-performed by rotating the piezo-driven plane mirror and keeping the beam-finding and focus positioning translation stages fixed. The piezo-driven mirror has a maximum angular scan range of 2.5 mrad , which corresponds to a position shift at the IP of $1250 \mu \mathrm{~m}$; which is suitable for positron bunch sizes smaller than $200 \mu \mathrm{~m}$.
- Stage scan-performed by moving the beam finding translation stage and keeping the piezo-driven mirror and focus positioning translation stage fixed. The stage used for moving the beam-finding translation stage has a maximum scan range of 50 mm and a minimum step size of $1 \mu \mathrm{~m}$. This scan type may be used to scan bunch sizes greater than $200 \mu \mathrm{~m}$.

The position of the laser focus relative to the positron beam can be moved by the focus positioning translation stage, as explained in Section 2.1. Then either a ramp scan or stage scan may be performed to obtain the positron beam size.

### 3.1. Profile measurements

This section presents positron bunch size measurements in the vertical and horizontal axes. An example VP is shown in Fig. 13. This scan uses 30 laser positions and the signals from 30 laser shots are averaged for each position. At the laser repetition rate of 20 Hz a scan took 45 s to complete.

To extract the measured sigma of the scan, $\sigma_{\mathrm{m}}$, the data are fit to the sum of a Gaussian plus a constant pedestal. $\sigma_{\mathrm{m}}$ contains contributions from the laser profile as given by Eq. (1), the transverse size of the positron charge distribution, $\sigma_{e}$, and the jitter term as defined in Section 2.3.2 $\left(\sigma_{\mathrm{jitter}}\right)$. Here $\sigma_{\mathrm{jitter}}$ has been assumed to be constant and is taken from the results of a separate measurement;


Fig. 13. Vertical scan profile corresponding to the minimum data point of Fig. 14.


Fig. 14. Plot allowing the extraction of $\sigma_{\mathrm{e}}$ (from the minimum), $M^{2}$ and $W_{0}$ in the VP from collision data. The $W_{0}$ and $M^{2}$ values are in agreement with earlier measurements presented in Sections 2.2 and 2.3.1.
this is justified in this instance by its relatively small contribution to the final result. A full treatment of the jitter contribution can be found in Refs. [2,9]. Assuming all distributions are Gaussian we obtain the following equation:
$\sigma_{\mathrm{m}}=\left[\frac{W_{0}^{2}}{4}+\left(\frac{M^{2} \lambda\left(x-x_{0}\right)}{2 \pi W_{0}}\right)^{2}+\sigma_{\mathrm{e}}^{2}+\sigma_{\mathrm{jitter}}^{2}\right]^{1 / 2}$
where $x$ is the position of the laser focus and $x_{0}$ is the location of the positron bunch, both along the axis of laser propagation.

In order to determine $x_{0}$, a number of scans were performed for a range of values of $x$, as shown in Fig. 14, and $x_{0}$ extracted from a fit to Eq. (3). Once the minimum is found, $\sigma_{\mathrm{e}}$ is extracted from scans taken at $x=x_{0}$.


Fig. 15. Horizontal scan profile corresponding to the minimum data point of Fig. 16.


Fig. 16. Plot allowing the extraction of $\sigma_{\mathrm{e}}$ (from the minimum), $M^{2}$ and $W_{0}$ in the HP from collision data. The $W_{0}$ and $M^{2}$ values are in agreement with earlier measurements presented in Sections 2.2 and 2.3.1.

A similar procedure was performed for the HP as shown in Figs. 15 and 16. The extracted positron beam dimensions are $(46.5 \pm 0.6) \mu \mathrm{m}$ in the vertical and $(377.3 \pm 3.0) \mu \mathrm{m}$ in the horizontal.

## 4. Conclusion

The PETRA LW system has successfully performed horizontal and vertical beam size measurements.

It has successfully employed an automated technique both to find the beam and to optimize the focus position; this made it possible to perform fast beam measurements in a manner that is non-invasive to normal accelerator operation.

It has performed precision beam size measurements, using a laser spot size of $W_{0} \simeq 9 \mu \mathrm{~m} \quad\left(\sigma_{0} \simeq 4.5 \mu \mathrm{~m}\right)$. Relative vertical positron beam size errors of $1.3 \%$ have been be achieved in a global multi-scan measurement (Fig. 14), where single scans can be performed in less than 50 s ; this could be improved by a higher laser repetition rate.

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